



Smart X-ray Optics

Smart X-ray Optics for the next generation of X-ray telescopes.

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Presentation Outline

Introduction

- Smart X-ray Optics Consortium
- The design of an active X-ray prototype

Prototype manufacture

- Mandrel production
- Electroforming procedure
- Actuator bonding/harnessing

Actuator influence functions

- Influence function measurements
- Hysteresis within the piezoelectric actuators

Software development

- Finite element analysis of actuator influence functions
 - An iterative algorithm to control actuator voltages

X-ray testing of the active prototype

• The X-ray tunnel test facility at the University of Leicester





The Smart X-ray Optics Project

The Smart X-ray Optics Consortium

- University College London
- University of Leicester
- University of Birmingham
- King's College London
- STFC Daresbury Laboratory
- University of Edinburgh
- Mullard Space Science Laboratory (MSSL)

Goals of the Smart X-ray Optics Consortium

To develop a prototype X-ray telescope with sub arc second resolution and potentially large filling factor whose optical form is actively controllable.



Figure 1: The Crab Nebula as imaged by three different x-ray telescopes, a) The Einstein Observatory (courtesy of NASA), b) ROSAT (courtesy of S. L. Snowden USRA, NASA/GSFC) and c) Chandra (courtesy of NASA/CXC/SAO)

To improve the resolution beyond that of the Chandra X-ray Observatory while increasing the available collecting area.





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An Active X-ray Prototype

Point-to-point X-ray focussing prototype

- Nickel ellipsoid (semi major axis ~14m) segment (300 x 100 mm)
- 30 curved piezoelectric actuators, developed by the University of Birmingham
- To be tested in the X-ray Tunnel Test Facility at the University of Leicester.
- Support of the optic within X-ray facility is designed by MSSL.

A cylindrical pre-prototype

- Nickel cylindrical segment (200 x 100 mm)
- Radius of curvature 154 mm
- Thickness 0.4 mm
- To be tested optically to determine actuator influence functions.





An Active X-ray Prototype

- Optical testing and prototype functionality to be tested at University College London
- X-ray testing to be performed at the University of Leicester's X-ray Tunnel Test Facility

Ray tracing of the optic within the test facility at Leicester, the majority of the X-rays miss the optic, however those incident upon the surface are reflected to the detector.





-1 0 1



The optic mount used to hold and manoeuvre the optic within the X-ray tunnel test facility





Prototype Manufacture: production method I



Cylindrical Mandrel

- Material: stainless steel
- Ground to a radius of curvature of 0.154m
- Surface roughness: 5nm rms

Elliptical Mandrel

- Material: aluminium coated with Kanigen
- Ground to a radius of curvature between 0.165m and 0.169m
- Expected surface roughness: 1nm rms
- Gold will be vacuum deposited upon the Kanigen surface to provide an passivation layer for the nickel deposition.

Mandrel polishing



Electroforming preparation



Electroforming Preparation

• Polyester insulating tape used to mask off the undesired regions.

• A thin polypropylene insulator is used to isolate the electroformed optic from the excess over plated regions.

• The electrical connection is via the two stainless steel supporting rods.



Prototype Manufacture: production method II

Electroforming



- A nickel sulphamate procedure
- Total plating time 40
 hours
- Operated at low current density 0.01A/cm²
- Mechanical agitation is provided by a filtering pump.





Release from the mandrel



Actuator bonding



- Actuators are bonded using a low shrinkage adhesive
- The adhesive contains small glass beads, which ensure that a minimum thickness layer is maintained.

 \bullet The glass beads are available in either 80 μm or 150 μm diameters





The completed cylindrical prototype



• Actuators harnessed to a 37 pin connector.

• Vacuum compatible acrylic adhesive tape is used to bind the wires.

• All 30 actuators have a common ground that can be set between a voltage range of -200 to 200 V.





- The mean radius of curvature is 0.182m
- The designed radius of curvature is 0.155m





Actuator Influence Functions



• Initial influence function measurements taken using an optically flat glass slide. On the back of which was bonded an actuator created by the University of Birmingham.

• Measurements were taken using a WYKO infrared interferometer and a Talysurf Profilometer.

• The visible area in the movie is 2.5 cm².

Piezoelectric hysteresis

• As the actuators are voltage driven; hysteresis is evident in the measurements.

- This is highly undesirable for precision and repeatability.
- \bullet The maximum difference in displacement is approximately 2 $\mu m.$





Actuator Influence Functions - Hysteresis



• By oscillating around the desired voltage, the effect of hysteresis is observed to be reduced.

• A control program was designed in LabVIEW to oscillate for approximately 4 minutes before stabilising on the desired voltage.

• Measurements of the displacement against voltage were obtained from actuators bonded upon the nickel shell.

• This method provided repeatability with an error of 1% in measured displacement.

Voltage varied between 0 and 100V.
A 30µm displacement was measured at 100V.



• A non linear relationship was measured for voltage against displacement in 20V steps.





Actuator Influence Functions - FEA





Software Development

- An approximated simulated annealing method
- Start with a distorted optic
- Try to improve the resolution using actuation



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Software Development



- A series of basis patterns are created using a Fast Fourier transform.
- These are then combined with the actuator influence functions to create the optic distortion.
- The routine iterates through the basis patterns and calculates the best combination.
- This creates the final actuator distortion of the optic.



Software Development





- Sine wave amplitude: 3 µm
- Initial HEW: 31.1 arcsec
- Final HEW: 30.1 arcsec
- number of iterations: 16



 Using radius of curvature measurement data from the cylindrical prototype scaled for the elliptical prototype.

fteration 11 12 13 14 15 16 17

FFT pattern - Initial optic sag

An improvement of 1 arcsec

- Initial HEW: 35.62 arcsec
- Final HEW: 34.65 arcsec
- number of iterations: 17



Operation within the X-ray environment





Testing at Leicester

- Test date: November 2008 for 4 weeks
- Test facility specifications: 28m in length

Energy range 0.1KeV to 100KeV Optional addition of a laser for alignment purposes MCP detector with 0.8m travel

Source end of the test facility

Optic mounting and a CAD drawing with the optic in place









Summary

The Smart X-ray Optic Consortium Goals

• To produce an active X-ray focussing optic with a resolution of 0.1"

Summary

- Completion of all the components of the X-ray tunnel facility mount.
- The cylindrical prototype has been fabricated and is awaiting testing.
- Actuator influence functions and the effects of hysteresis have been investigated.

• A simulated annealing method has been combined with simulated and measured data to provide the control of the actuators.

Current and Future Work

- The elliptical mandrel is in the final stages of completion
 - Further tests in the investigation of hysteresis.
 - Cylindrical prototype actuation testing.
 - Elliptical prototype manufacture and completion.

Target

 To produce the active elliptical prototype by the 1st Nov 2008, ready for testing in the University of Leicester's X-ray beam facility





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