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Emittance Measuremet on the CeB_6 Electron Gun for the SPring-8 Compact SASE Source

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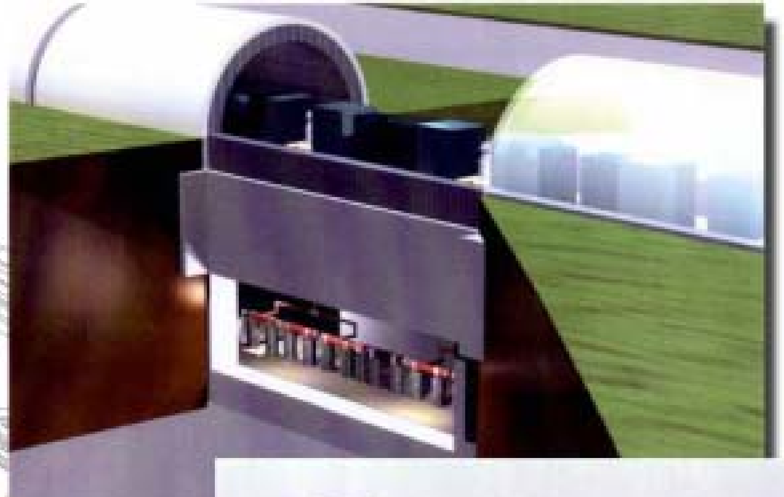
Future X-ray FEL (Image View)

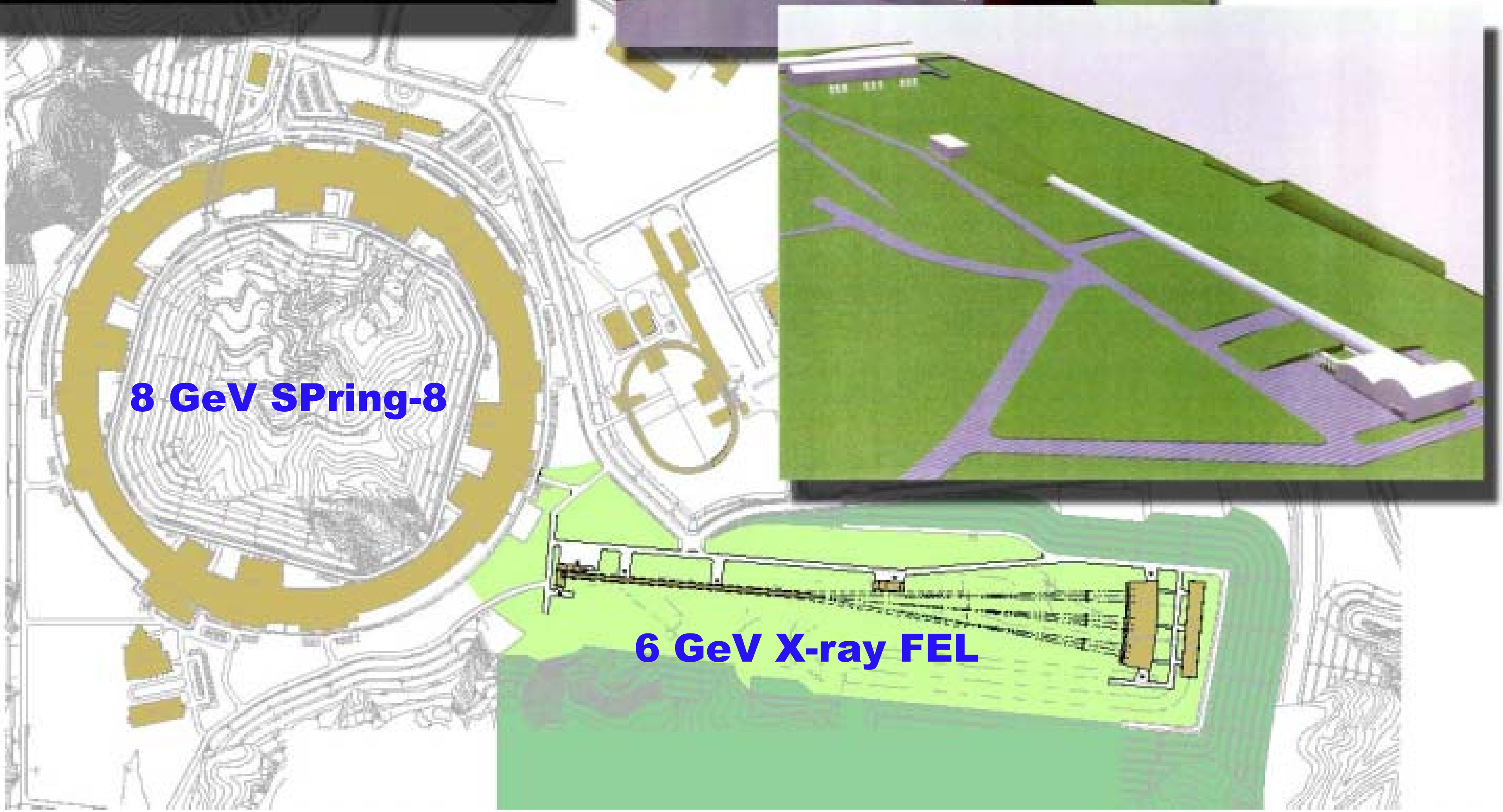
6 GeV C-band Accelerator

1 Å Target Wavelength

1 km Site length

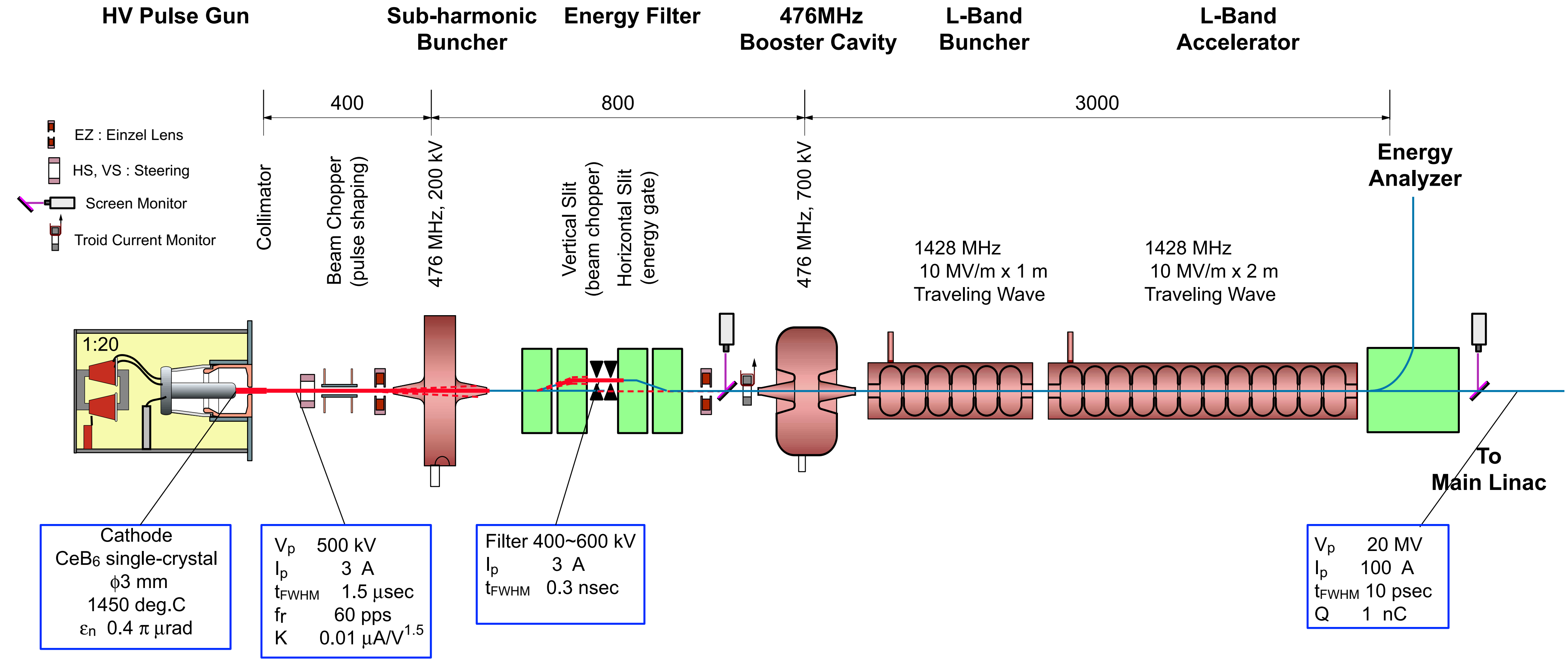
Multiple User Beam Lines





2002 July

Low Emittance Injector for SASE-FEL



CeB_6 Cathode Development

Choice of Cathode Material

X-FEL Requirements

Very Low emittance

$\varepsilon_{n,rms} \leq 1\pi\ mm.mrad$ - - - - - - - ➤

High Beam Current at Gun

$I_p \sim 3A$ - - - - - - - ➤

Long Lifetime

>10,000 hours - - - - - - - ➤

Thermal Emittance

$$\varepsilon_{n,rms} = \frac{r_c}{2}\sqrt{\frac{k_B T}{m_e c^2}}$$

⇓

Small Cathode

$r_c \leq 2mm$

$T = 1000 \sim 1500°C$

⇓

High Emission Density

$j_c \sim 50A/cm^2$

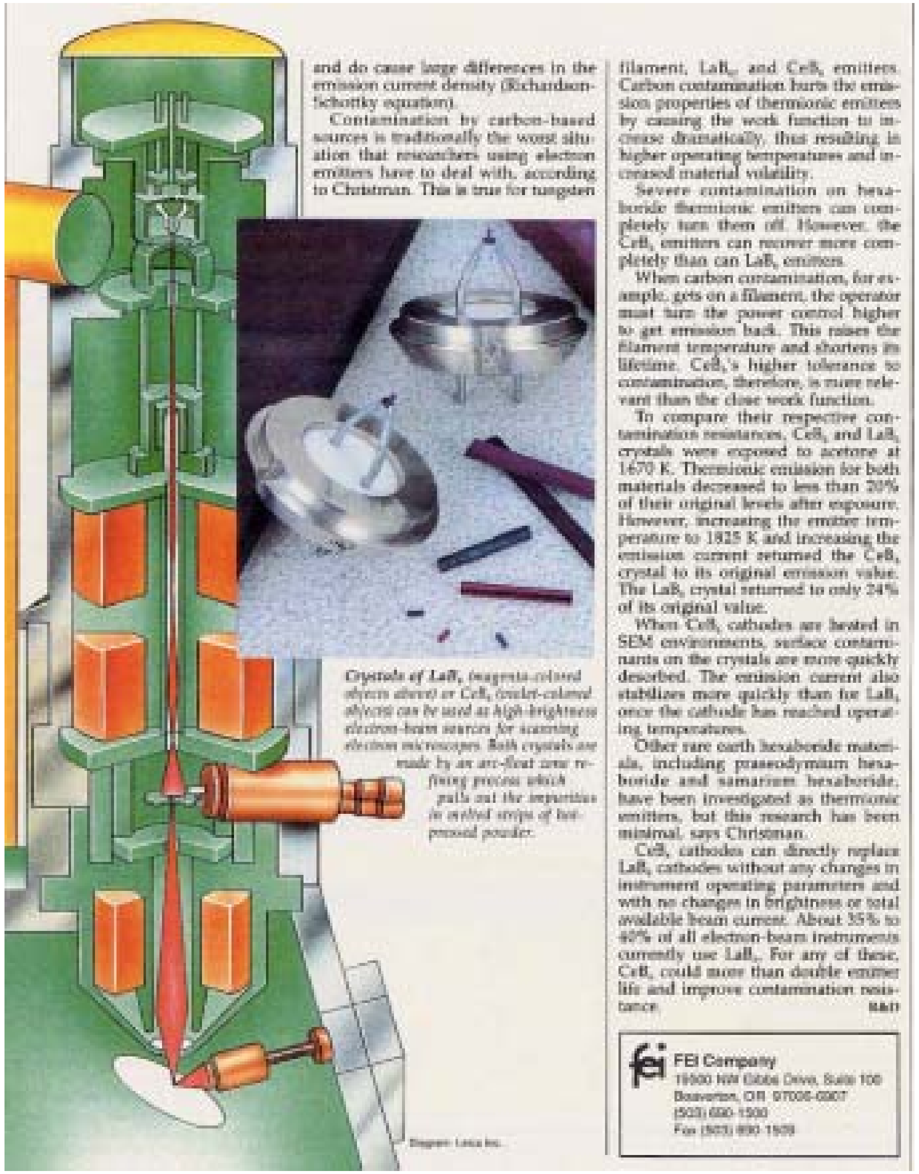
⇓

Rare-earth Hexaborides

LaB_6 or CeB_6

CeB_6 (Cerium Hexaboride) Single-Crystal Cathode

CeB_6 cathode is widely used in electron microscope !!



and do cause large differences in the emission current density (Richardson-Schottky equation).

Contamination by carbon-based sources is traditionally the worst situation that researchers using electron emitters have to deal with, according to Christman. This is true for tungsten filament, LaB_6 and CeB_6 emitters. Carbon contamination hurts the emission properties of thermionic emitters by causing the work function to increase dramatically, thus resulting in higher operating temperatures and increased material volatility.

Severe contamination on hexaboride thermionic emitters can completely turn them off. However, the CeB_6 emitters can recover more completely than can LaB_6 emitters.

When carbon contamination, for example, gets on a filament, the operator must turn the power control higher to get emission back. This raises the filament temperature and shortens its lifetime. CeB_6's higher tolerance to contamination, therefore, is more relevant than the close work function.

To compare their respective contamination resistances, CeB_6 and LaB_6 crystals were exposed to acetone at 1670 K. Thermionic emission for both materials decreased to less than 20% of their original levels after exposure. However, increasing the emitter temperature to 1825 K and increasing the emission current returned the CeB_6 crystal to its original emission value. The LaB_6 crystal returned to only 24% of its original value.

When CeB_6 cathodes are heated in SEM environments, surface contaminants on the crystals are more quickly desorbed. The emission current also stabilizes more quickly than for LaB_6 once the cathode has reached operating temperatures.

Other rare earth hexaboride materials, including praseodymium hexaboride and samarium hexaboride, have been investigated as thermionic emitters, but this research has been minimal, says Christman.

CeB_6 cathodes can directly replace LaB_6 cathodes without any changes in instrument operating parameters and with no changes in brightness or total available beam current. About 35% to 40% of all electron-beam instruments currently use LaB_6. For any of these, CeB_6 could more than double emitter life and improve contamination resistance. R&D

Crystals of LaB_6 (magenta-colored objects above) or CeB_6 (violet-colored objects) can be used as high-brightness electron-beam sources for scanning electron microscopes. Both crystals are made by an arc-float zone refining process which pulls out the impurities in melted strips of hot-pressed powder.

Diagram: Leica Inc.

Properties

- Very flat surface
  (surface roughness <1 μm)
- Low workfunction (~2.4 eV)
- Long lifetime (>10,000 hours)
- Rapid recovery from contamination

Design parameter of SCSS cathode

- Thermal Emittance

$$\varepsilon_{n,rms} = \frac{r}{2}\sqrt{\frac{k_B T}{m_e c^2}} = 0.4\,\pi\ \text{mm mrad}$$

Cathode Radius $r = 1.5$ mm

Temperature $T = 1450$ (1723 K)

- Emission Current Density

Richardson-Dashman's Formula (Ideal Case)

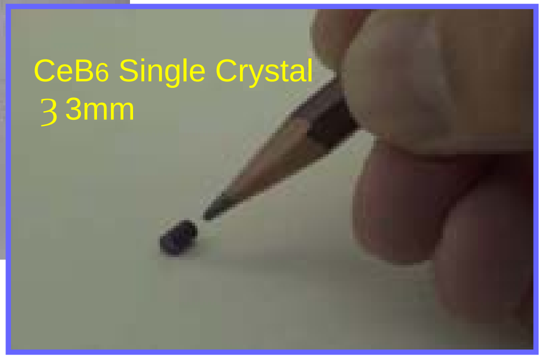
$$J = 120.4\ T^2 \exp(-\phi' / k_B T) > 42\ \text{A/cm}^2$$

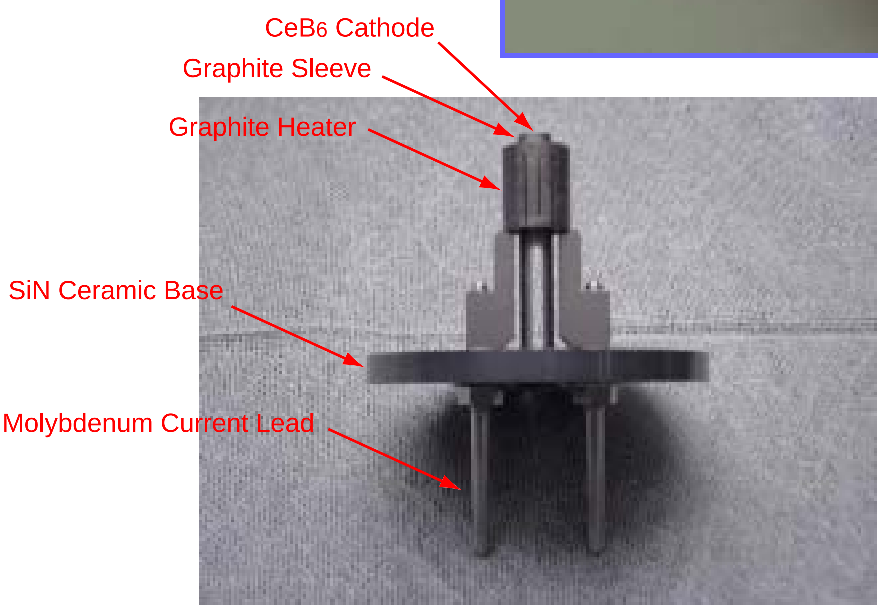
Boltzmann's Constant $k_B = 8.617 \times 10^{-5} (eV / K)$

Effective Workfunction $\phi' = \phi - \frac{e}{2}\sqrt{\frac{eE}{\pi\varepsilon_0}}$ ~2.3 (eV)

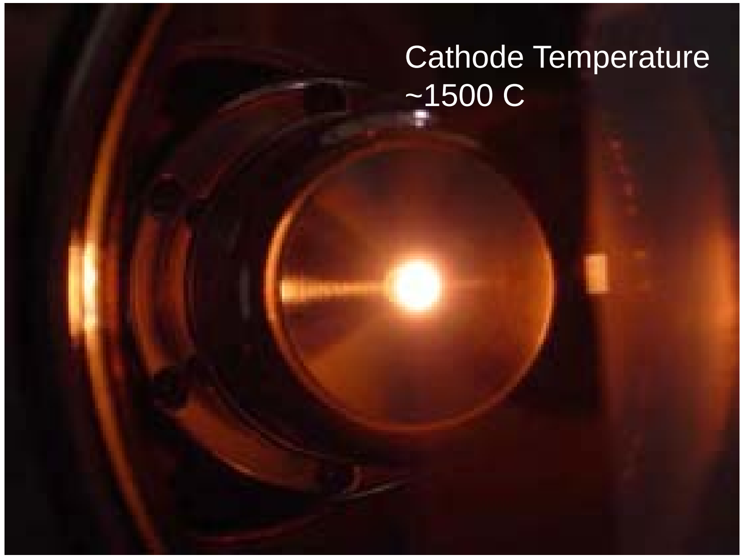
CeB_6 Cathode Assembly (New Model)

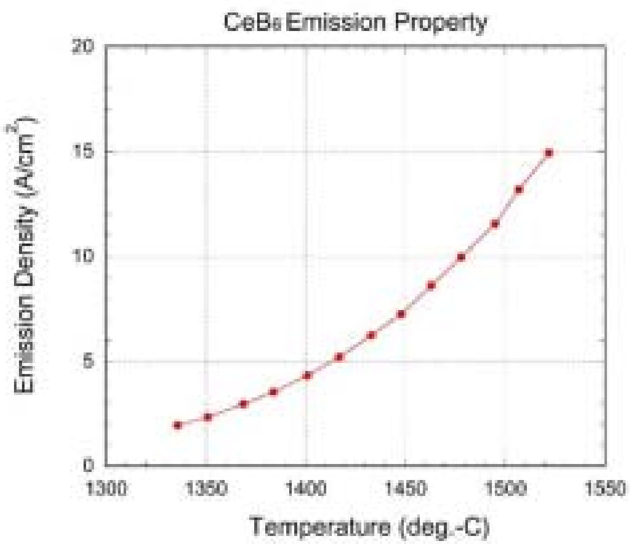
Cathode Assembly





Heated Cathode in Stem



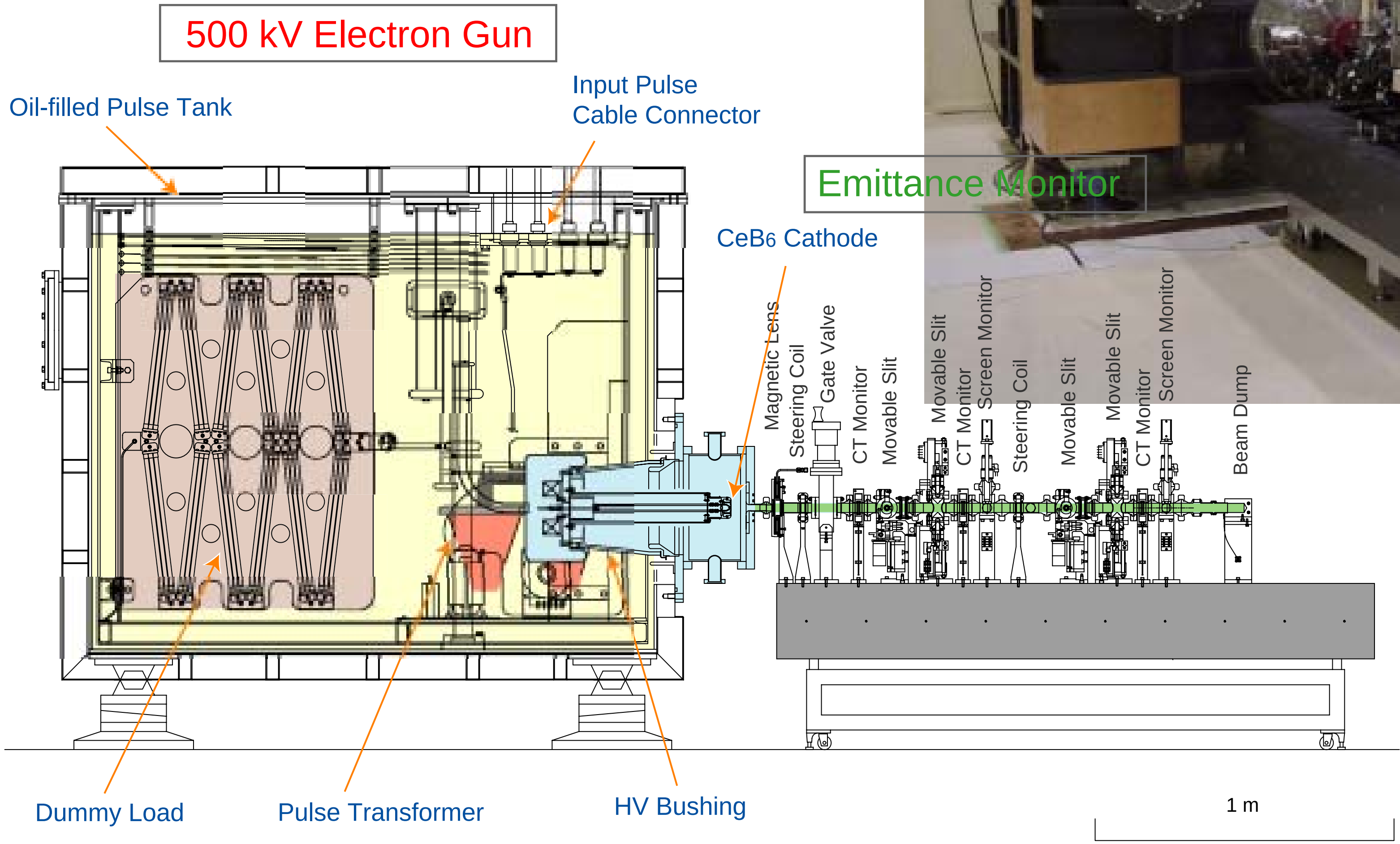


The gun voltage=500 kV
Temperature was measured at the graphite sleeve by a radiation monitor.

500 kV Electron Gun

500 kV Electron Gun

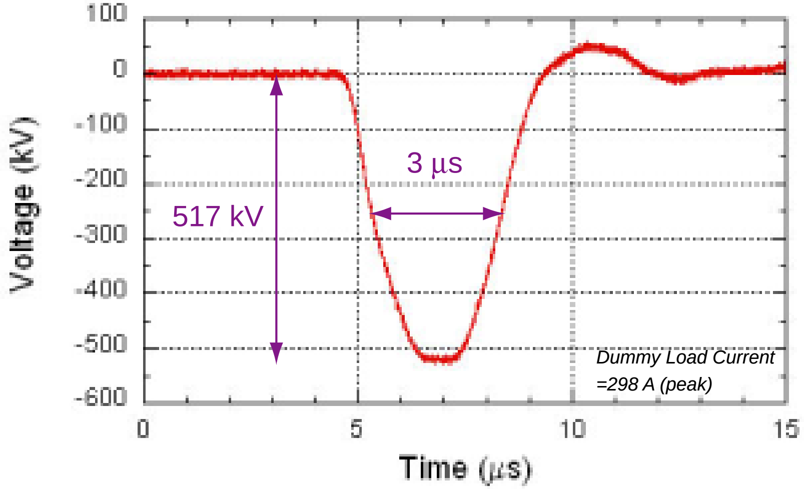
C-band klystron modulator is used as a HV pulsed power supply.



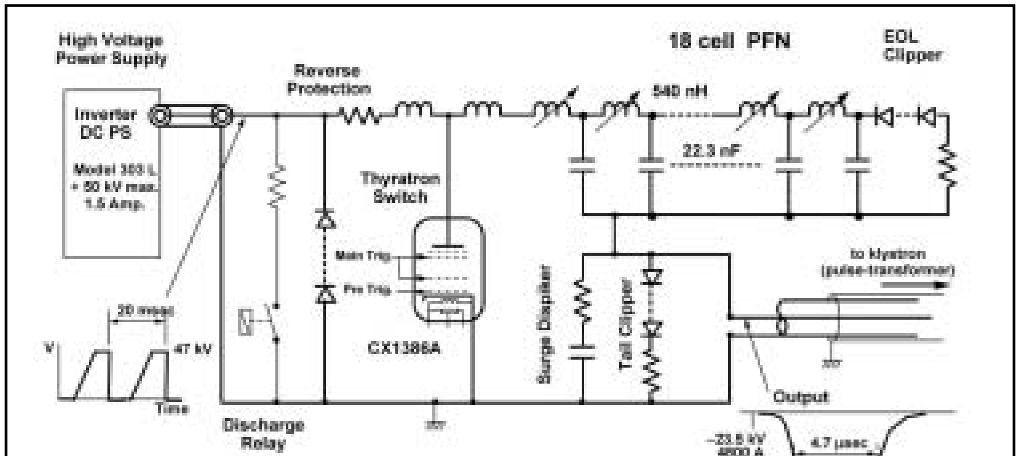
C-band Klystron Modulator

Same model of the C-band klystron modulator is used for the 500 kV electron gun.

Gun Pulse Waveform

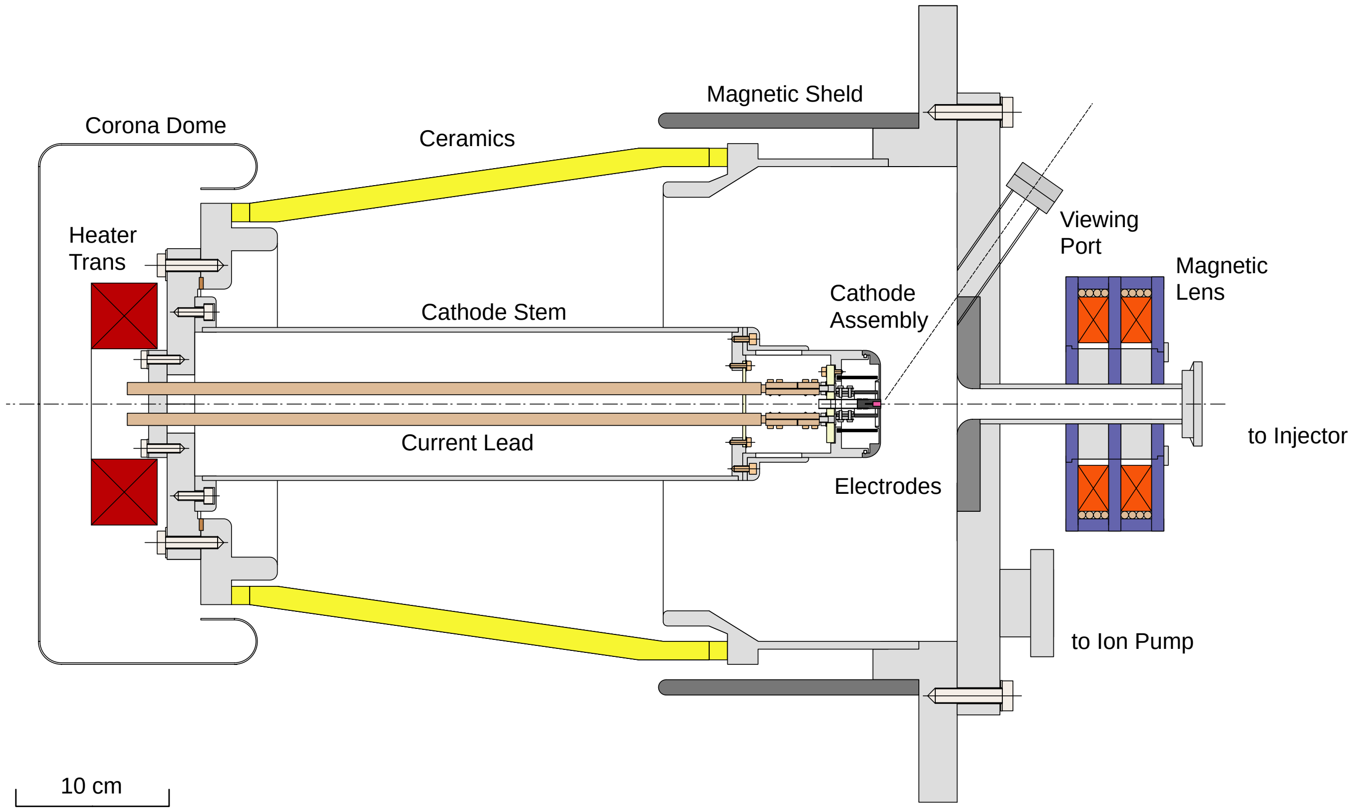


Circuit Diagram



PFN : 13 section (for 500 kV Gun)
PFN Impedance : ~4 Ω
Charging Voltage : 50 kV max
Max. Repetition Rate : 60 pps

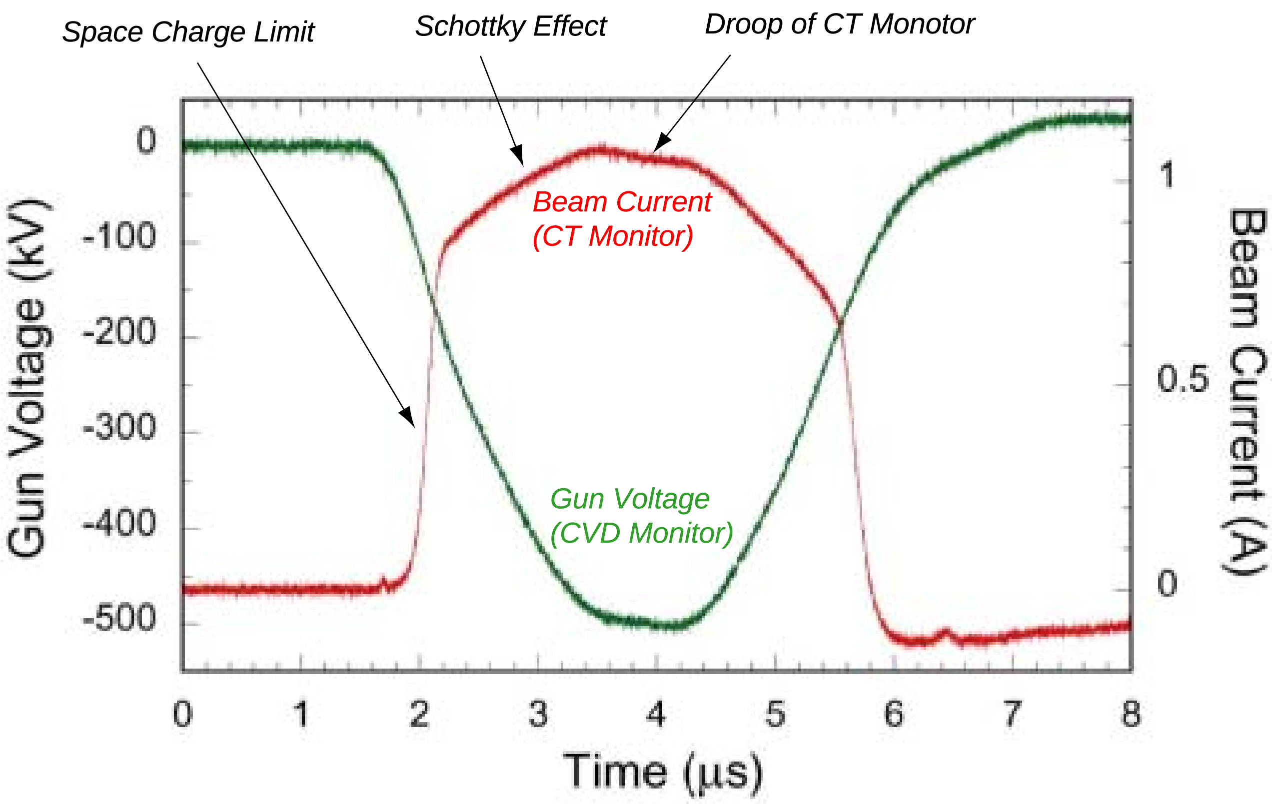
500 kV Electron Gun Chamber



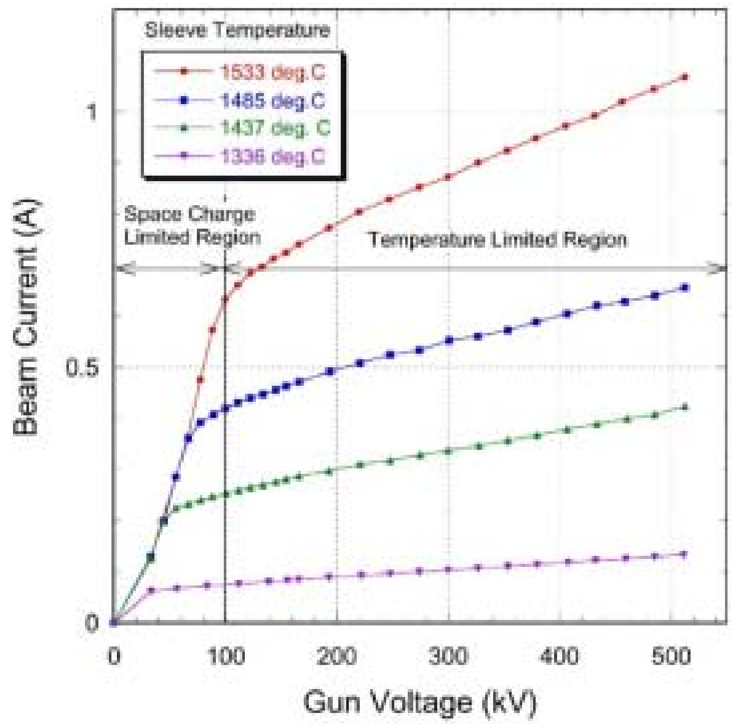
Conceptual Design (2001)

500 keV Beam Production

Beam Waveform



I-V Curve



~1 ns part will cut out from the flattop by a beam deflector, and be used for the SCSS accelerator.

We operate the gun in temperature limited region to reduce emittance growth due to space charge.

Emittance Measurement

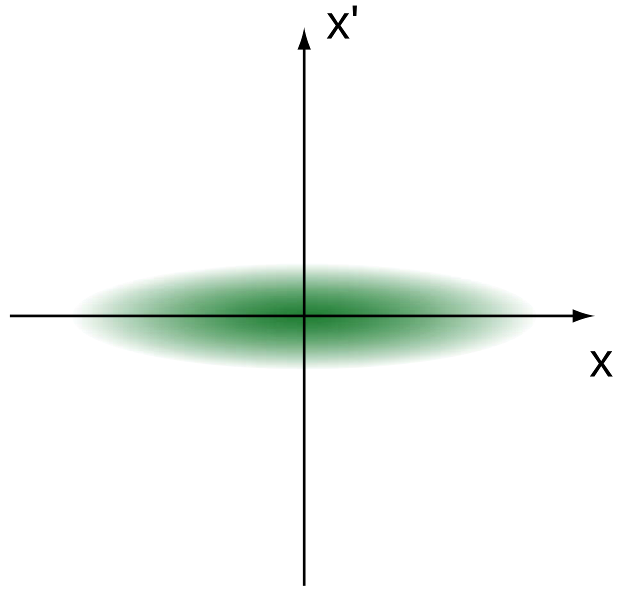
Normalized rms Emittance

Definition

$$\varepsilon_{n,rms} = \frac{1}{m_0 c}\sqrt{\langle x^2\rangle\langle p_x{}^2\rangle - \langle x\cdot p_x\rangle^2}$$

$$= \beta\gamma\sqrt{\langle x^2\rangle\langle x'^2\rangle - \langle x\cdot x'\rangle^2}$$

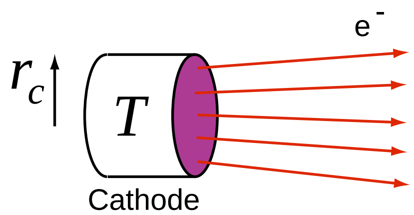
unit : π mm.mrad



$$\langle x^2\rangle = \frac{\int\int x^2 i\,(x, x')dxdx'}{\int\int i\,(x, x')dxdx'}$$

$$\langle x'^2\rangle = \frac{\int\int x'^2 i\,(x, x')dxdx'}{\int\int i\,(x, x')dxdx'}$$

$$\langle x\|x'\rangle = \frac{\int\int x\|x' i\,(x, x')dxdx'}{\int\int i\,(x, x')dxdx'}$$

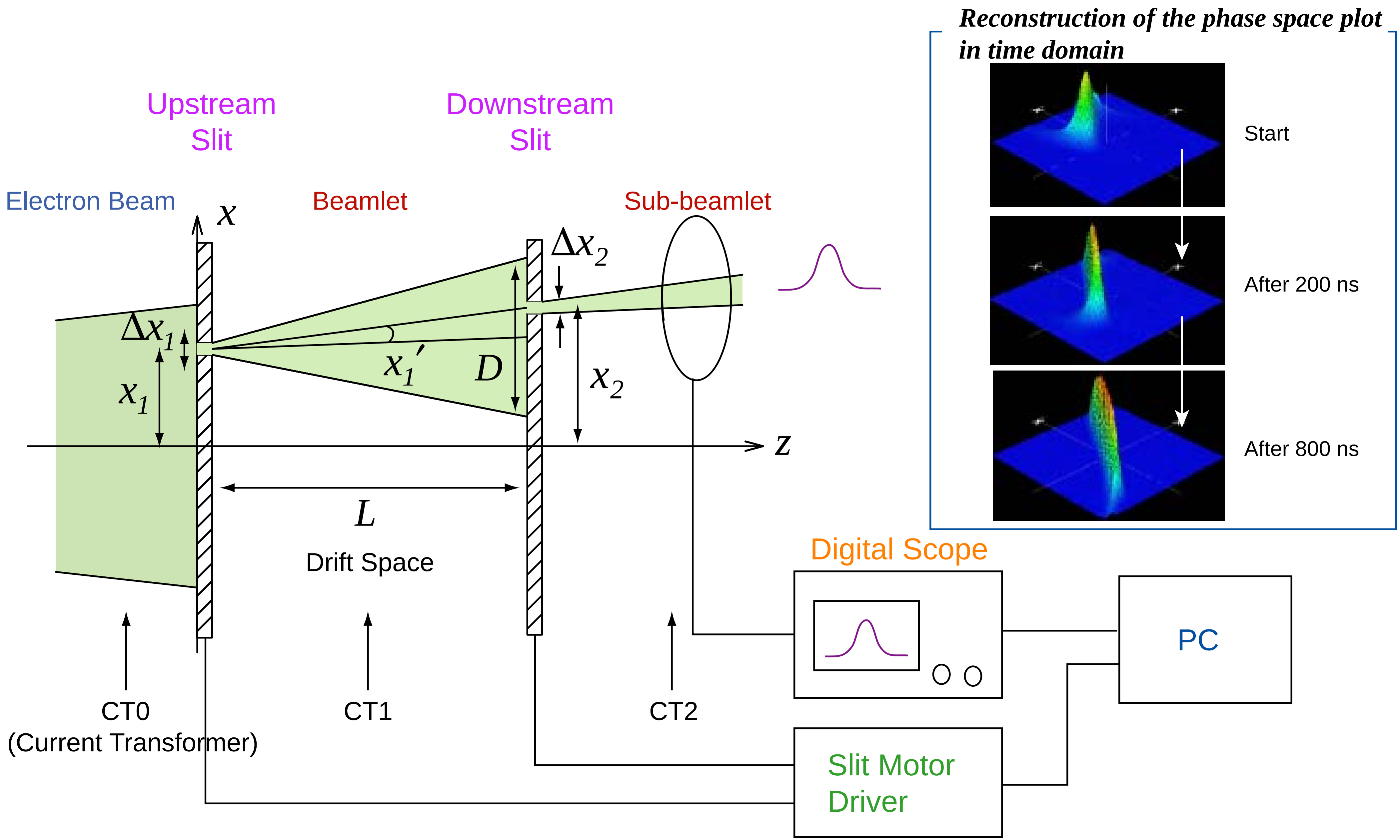


$$\varepsilon_{n,rms} = \frac{r_c}{2}\sqrt{\frac{k_B T}{m_0 c^2}}$$

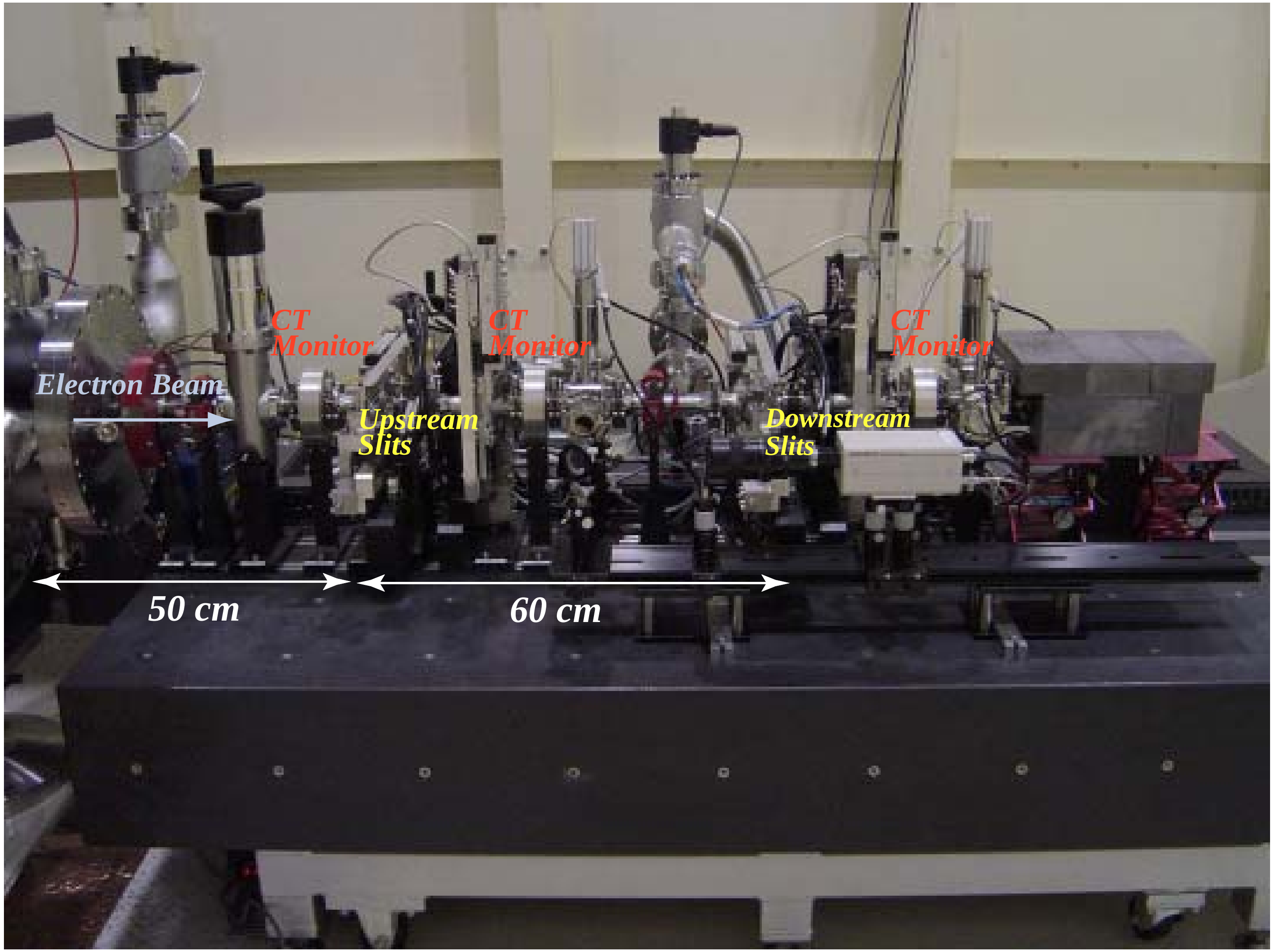
= 0.4 π mm.mrad

(r_c = 1.5 mm, T = 1723 K (1450 ή ((

Emittance Measurement by Double-slits

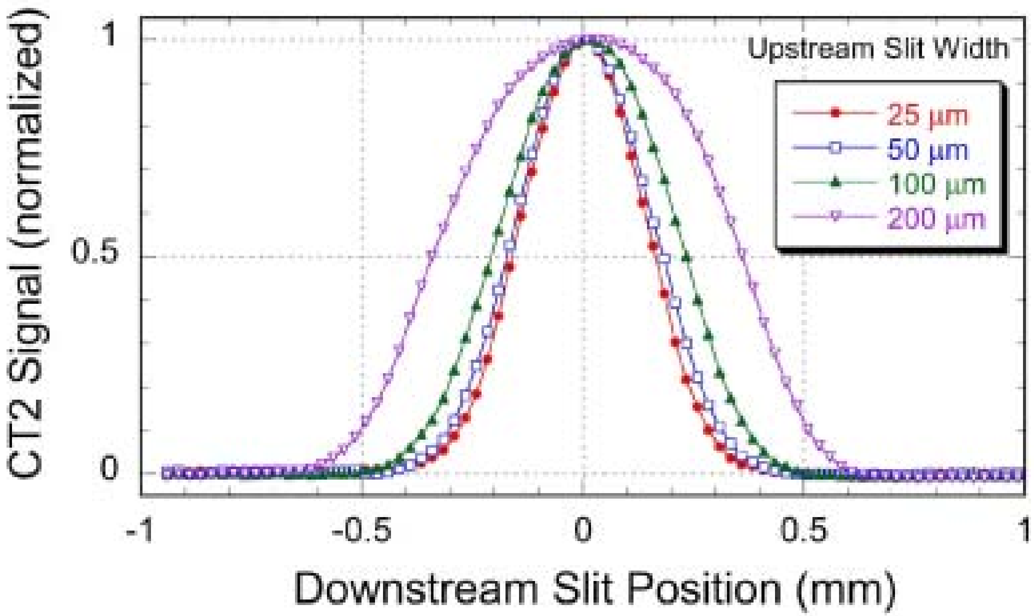


Emittance Monitor

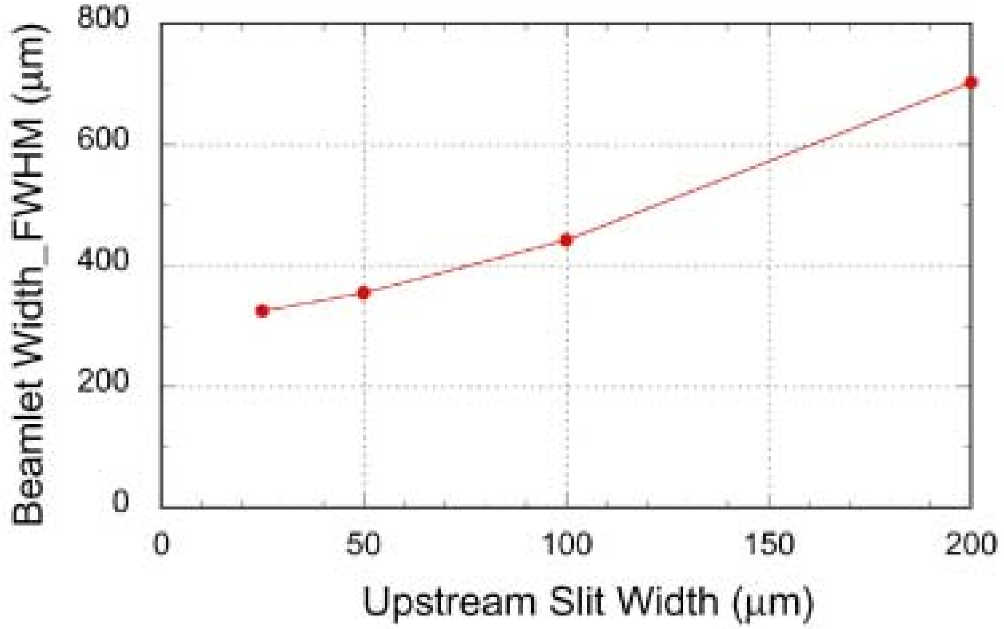


Beamlet Spreading due to Space Charge

Beamlet Profiles (400 keV, 0.9 A)



Beamlet Width (FWHM)



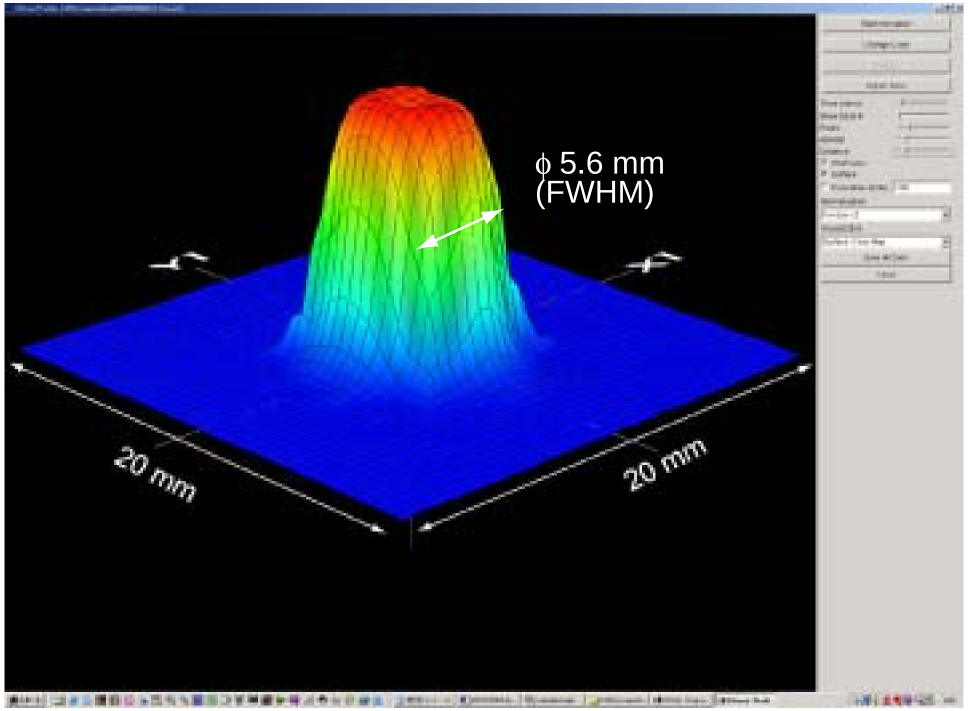
Beamlet spreads due to not only the thermal momentum but also the space charge force.

Opening width of the upstream slit must be narrow enough that the space charge effect can be neligible.

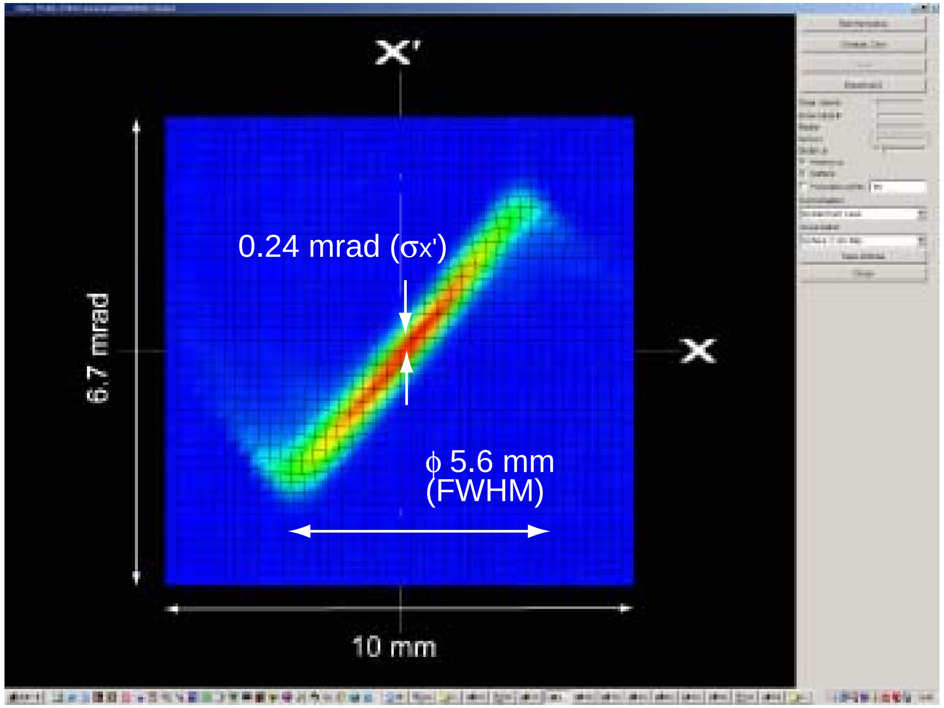
Beamlet spread due to space charge is about 15% at 50 µm width.

Emittance of 500 keV Beam

Beam Profile



Phase Space Profile



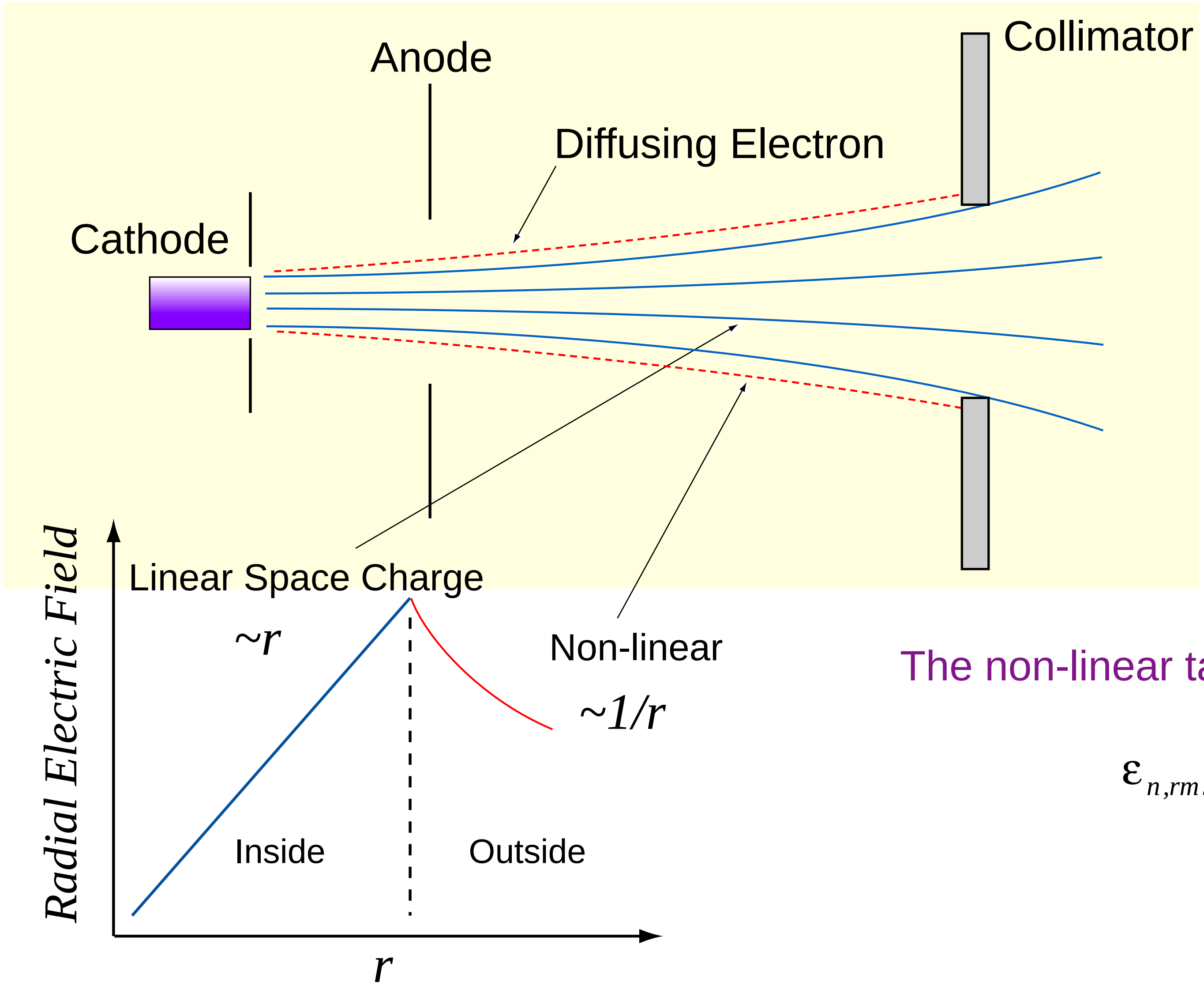
Beam Energy : 500 keV
Peak Current : 1.0 A
Pulse Width : 3 μs

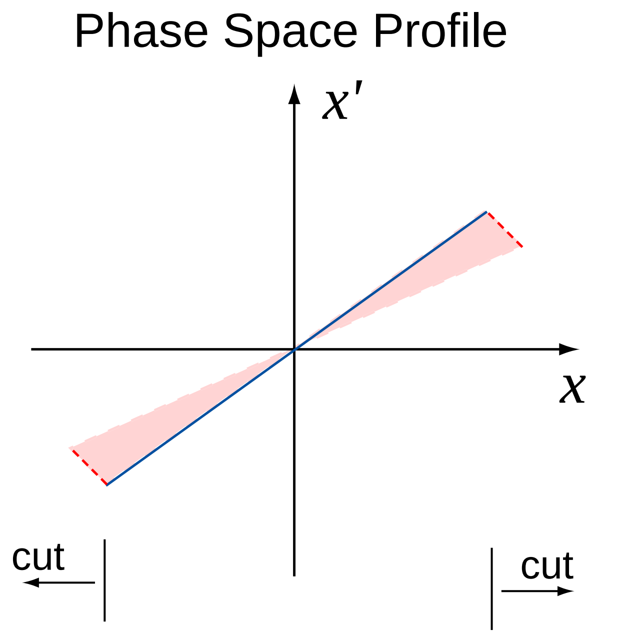
Emittance ($\varepsilon_{n,rms}$)

Requirement : ≤1π mm.mrad

Experiment : 1.1π mm.mrad

Emittance with Thermal Diffusion and Non-linear Space Charge





The non-linear tail can be removed by collimator.

$$\varepsilon_{n,rms} = \beta\gamma\sqrt{<x^2><x'^2> - <xx'>^2}$$

$$= \beta\gamma\cdot\sigma_{x'}\cdot r/2$$

$$= 1.707 Ö 0.24\ mrad Ö 1.4\ mm$$

$$= 0.6\,\pi\ mm.mrad\ \ (expected)$$

Electrons diffuse to the outside by thermal motion.
Non-linear space charge force breaks emittance.

Summary

1) *We have succeeded in producing a 500 keV, 1 A beam from the CeB_6 gun.*

2) *Measured emittance was ~1π mm mrad.*

3) *In 2004, we will install a beam deflector and a buncher system, and measure the bunched beam emittance.*